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FIRE CONTROL ANALYSIS OF SELECTED CREW SERVED WEAPONS

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U.S. ARMY ARMAMENT RESEARCH, DEVELOPMENT AND ENGINEERING CENTER

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Picatinny Arsenal, New Jersey

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INTRODUCTION

A study has been made of the accuracies that are attained by using four different fire control systems on each of several small arms. Its purpose is to get exact information about the relative advantages of these systems. The results of this study should, therefore, make it easier to decide intelligently what fire control system to provide for what weapon. Here, "accuracy" means the standard deviation of the angle, measured at the shooter, between the bullet's point of impact and the point that the shooter wants to hit.

In this study, it was assumed that no fire control system has a fixed bias, that the mean point of impact over a long period of time was the "bull's eye" in every case. It was then reasonable to model the probability density function of the bullet's angular dispersion as a two-dimensional normal distribution, the standard deviations of which are the bullet's accuracies in the horizontal and vertical directions. Probabilities of hit on a standard NATO target were then calculated for every fire control system, weapon, and range by a computer program that is based on this model (ref 1). The probabilities of hit (app A) were based on error budgets that were developed for quasi-combat conditions. The probability of hit is the ultimate figure of merit for a fire control system.

ANALYTICAL APPROACH

The different error sources were divided into occasion-to-occasion errors and round-to-round errors.

Occasion-to-occasion errors are errors which change so slowly that they can be considered to be constant throughout an engagement. The occasion-to-occasion errors that were calculated were errors in range to the target, wind speed and direction, muzzle velocity, air temperature, air density, boresighting, fire control solution and zeroing, together with failure to take account of the gun's cant, earth rate, site angle, reticle gradations and jump dispersion.

Ignorance or error about the target range or the wind velocity will clearly produce errors in aiming.

Muzzle velocity varies according to the temperature of the propellant. An error in muzzle velocity will, therefore, produce an error in aiming especially if the target is moving.

Air temperature determines propellant temperature, which in turn affects muzzle velocity.

The gun and sighting system must be optically aligned, that is to say, boresighted to provide accurate firing. Repeated firings and other vibration will cause deviations from this alignment. This is the boresight error.

The solution that is provided by the fire control system will contain some error because of approximations and tolerances in construction. This is the fire control solution error.

A gun is zeroed by shooting several times at a target that is a known distance from the gun and adjusting the fire control system so that these shots fall on the target. Atmospheric conditions will probably be nonstandard when this is done. Also only a few shots are fired for zeroing; so there will probably be an error in zeroing.

Errors are introduced into the superelevation calculations when the vehicle is canted because of uneven terrain. The same sort of error occurs when the gun is handheld for it will probably not be held perfectly vertical. This is the cant error.

Earth rate errors are caused by not taking the Coriolis force into account. This error is quite small but it has been included in the analysis all the same. If the gun and target are not at the same elevation, the fact that the trajectory of a round is not rigid causes a site-angle error. The profile of the trajectory cannot simply be tilted to the target's elevation and keep its original shape. The amount of error is small at low ranges but becomes important as range increases.

A reticle is a set of lines or cross-hairs on a sight, each of which corresponds to a certain range and gives the correct superelevation for that range. But if the target's range is not one of those that are marked on the reticle, the shooter will have to estimate the superelevation. This error in doing so is the reticle error.

Jump dispersion error is the net result of unknown combinations of error which are present at all firings and are constant for a particular vehicle, gun, and ammunition lot. This is a fixed bias which is corrected in any fire control system. But there is a residual variable jump dispersion error which is one of the occasion-to-occasion errors.

It was assumed that all of the above sources of error were statistically independent and that the horizontal and vertical components of each source of error were statistically independent. Therefore, considering only horizontal components of error, the variance of the occasion-to-occasion error is the sum of the variances of all the sources of such error. The same holds for the variance of the vertical component of the occasion-to-occasion error. This is how the variances of both components of the occasion-to-occasion error were calculated.

In contrast to occasion-to-occasion errors, round-to-round errors change, as the name implies, from round to round. Round-to-round errors are random, taking on different values for every round so that no correction can be made by the fire control system. The round-to-round errors that were considered were ammunition dispersion and errors in aiming and resolution.

Ammunition dispersion is due to the number and size of the propellant grains in the projectile, the fit of the projectile to the case, the position of the round in the chamber, etc. It must be treated as a round-to-round error.

The resolution of an optical system is the smallest angle between two points which the system can still resolve, that is, recognize as two points rather than one. The resolution of the human eye is about 12 seconds of arc or 0.06 mil. This limited resolution of the eye is a source of error which, like the aiming error, varies from round to round.

There will be a randomly varying aiming error no matter how clearly the shooter sees the target. The point at which he aims is bound to wander a little.

As with the occasion-to-occasion errors, it was assumed that all sources of round-to-round error were statistically independent and that the horizontal and vertical components of each source of error were also statistically independent. The variances of the horizontal and vertical components of the round-to-round error were calculated by adding the variances of the horizontal and vertical components, respectively, of the error sources.

Naturally, most of these errors depend on range so it was necessary to make a separate calculation for every range to be considered. The ranges 200 m, 400 m, 600 m, and so on up to 2000 m were used in this study.

The computer program that calculates probability of hit is based on the following model (ref 1). For a given range, let the standard deviations of the horizontal and vertical components of the occasion-to-occasion error be SX and SY and of the round-to-round error be SXP and SYP. The program assumes that the impact points of the bullets have a two-dimensional normal distribution with standard deviations SXP and SYP and means mx and my. For their part, mx and my have a two-dimensional normal distribution with standard deviations SX and SY and means 0 and 0. This corresponds to the idea that we assume no fixed bias and that the temporary bias for one engagement is (mx, my), which is itself normally distributed. The program then calculates the probability of hit of a single bullet as the integral of this probability distribution over the target. The targets will be described in the next section.

EQUIPMENT STUDIED

The four fire control systems used in the analysis provided different amounts of compensation for system errors. They are described below in the order of increasing complexity.

System 1 consists of iron sights only. These are posts mounted on the barrel and breech of the weapon which are used to align the weapon and target. No other fire control instrument is employed. This system is the current level of equipment on the M2 and M60 machine guns.

System 2 consists of a telescopic sight, a stadia range finder and a ballistic reticle. The user of a stadia range finder must know the true size of the target. It may, for instance, be an enemy vehicle with which he is familiar. The stadia range finder then supplies the target's range from its angular size. Knowing the range to the target, the shooter can get the correct superelevation from the ballistic reticle.

System 3 consists of a telescopic sight, a laser range finder, and a ballistic reticle. A laser range finder is more accurate than a stadia range finder and so the user gets a better value of the superelevation from the ballistic reticle than he would with system 2.

System 4 consists of a telescopic sight, a laser range finder, a ballistic computer, and sensors for cross-wind speed, air pressure and air temperature, ammunition temperature, and weapon cant.

The ballistic computer calculates air density from the air pressure and temperature. The ammunition temperature is not precisely the temperature of the ammunition. It is the air temperature in the container where the ammunition is kept. Nonetheless, it is assumed that the error in muzzle velocity is reduced 40% by making use of this temperature. The cant of vehicle is rotation about a front-to-back axis. It is sometimes called trunnion roll.

The ammunitions studied are .50 cal M8 API (armor-piercing incendiary), the M20 API-T (armor-piercing incendiary-tracer), the M33 ball and the XM903 SLAP (sabot-launched, armor penetrating), all fired from the M2 machine gun; the 7.62 mm M80 ball and the XM948 SLAP, both fired from the M60 machine gun; and the M118 NM (national match) fired from the M21 and M24 sniper weapons.

The study assigned the NATO vehicle target, which is 2.3 m², to the AP and SLAP rounds. The target for the other rounds was a rectangle, 1 meter high and 1/2 meter wide, which represents a crouching man. It is similar to the NATO personnel target.

EXPLANATION OF ERROR BUDGETS

The error budgets list (app B) standard deviations of angular error. The unit for all of them is the Army mil, where 6400 Army mils = 360 degrees = 2π radians. The standard deviations of the horizontal and vertical components of error have been calculated separately and are listed separately under the column headings H and V. These horizontal and vertical components of error were calculated for every target range from 200 m to 2000 m at intervals of 200 m and are presented as a pair of H and V columns headed by the range. The rest of this section will be devoted to explaining the calculation of all the kinds of errors that appear in the error budgets.

Range Error

The error in a naked eye estimate of range is taken as 21%. Let R and E denote range and superelevation. Then the angular range error for system 1 is 0.21 R dE/dR (ref 2, pp. 32 - 33). The rate dE/dR depends on range and was calculated by Ballistic Research Laboratory (BRL) at the Aberdeen Proving Ground, MD (app C). This range error is in the vertical direction. The horizontal range error is zero for all systems.

The range error when using a stadia range finder is taken as 15%. It follows, using the same notation as above, that the range error for system 2 is 0.15 R dE/dR in the vertical direction.

System 3 and 4 have laser range finders for which the error is 10 m. So, for these systems, the vertical range error is 10 dE/dR.

Cant Error

Cant error is only in the horizontal direction. It was calculated from the formula CE = 0.001SC, where CE, S, and C are the cant error, superelevation and standard deviation of cant, all in mils (ref 2). The superelevation was calculated for each round and range by BRL (app C); C was 5 degrees for systems 1 through 3 for which there was no cant sensor and set at 0.5 degrees for system 4 which has a cant sensor.

Error Caused by Wind

The error caused by cross-range wind is entirely horizontal and is shown in the H column. On the other hand, the error caused by range wind is entirely vertical and so is shown in the V column. A mean value of 3.35 m/s was taken for both range and cross-range wind for systems 1, 2, and 3. The mean value of the range wind was also set at 3.35 m/s for system 4. But the cross-range wind was set at 1.75 m/s for system 4 since it has a sensor for cross-range wind. The error was found from the unit effects data at

the fixed range calculated by BRL (app A). For instance, let the round in question be the 7.62 mm ball M80. A 1 m/s range wind causes an increase of 0.0433 m in height at a range of 1000 m. So, a 3.35 m/s range wind causes an increase of 3.35 x 0.0433 m in height at the range, which is an angular error of 3.35 x 0.0433/1000 radians which is easily converted to mils.

Error in Velocity

The term velocity here refers to muzzle velocity. The angular deviation caused by an error in the muzzle velocity is in the vertical direction alone. The primary reason for variation in the muzzle velocity is variation in the temperature of the propellant. The mean error in the muzzle velocity was taken as 10 m/s in systems 1 through 3 and 2 m/s in system 4 which senses the temperature of the ammunition container.

The error was found from the unit effects data at a fixed range in the data from BRL. For instance, let E denote the change in height, measured in meters, which results from a 1 m/s change in velocity when the range is R. The mean angular error for systems 1 through 3 is then 10 E/R radians for systems 1 through 3.

Temperature Error

The temperature in question is air temperature. A change in air temperature will cause a change in propellant temperature, which in turn affects muzzle velocity, which, in turn, will affect the round's trajectory. Failure to take account of this results in a temperature error. This error is in the vertical direction.

The mean temperature error was taken as 5% of absolute temperature (Rankine or Kelvin temperature) for systems 1 through 3. The error was 1% of absolute temperature for system 4 which has a temperature sensor. This error is calculated from the data in appendix A, the same as the velocity error.

Air Density Error

A false value of air density will cause an angular error in the vertical direction. The mean air density error was taken as 5% of absolute air density for systems 1 through 3 and 1% of that for system 4, which senses air pressure and temperature.

This error is calculated from the data in appendix C, the same as the wind, velocity, and temperature errors.

Earth Rate

Because the earth is, in reality, a moving platform, firing a projectile from the earth introduces an error caused by Coriolis acceleration (moving bodies on moving frames of reference). The horizontal and vertical values for the error are:

$$X_F = -(\sin L) (\cos A)E$$

$$Y_c = -(\cos L) (\sin A)E$$

where

L is latitude (north, positive; south, negative)

A is azimuth (north, zero, clockwise)

E is Coriolis acceleration

$$E = \int_{0}^{t} \int_{0}^{p} 2/\phi \times V/dt ds$$

where

V is the shell's velocity vector (m/s)

t is the time of flight (sec)

While this integration looks forbidding, it can be accomplished graphically in a short time by plotting 2ϕ V against time and finding the area from zero to the time of flight for the range in question. Plotting this area against time and repeating the process yields the desired E.

In estimating the standard deviation, the placement of iand masses on the earth's surface suggests that the latitude readings will be biased toward the northern hemisphere while the azimuth is uniformly random in all directions. Since the azimuth is random and little more can be said about the likelihood of combat at any particular latitude, a value of 45 degrees has been chosen as OL and OA to minimize the error in both directions.

Consequently, the standard deviations of the horizontal and vertical components of the error are:

$$\sigma_{\rm X_c}$$
 = |E| (sin 45 degrees cos 45 degrees) = 0.5 |E|

$$\sigma_{Y_E} = |E| (\cos 45 \text{ degrees sin 45 degrees}) = 0.5 |E|$$

Site Angle

Site angle error was calculated by the formula SAE = SE (1-COS T) where SAE, SE, and T denote site angle error, superelevation, and a terrain feature similar to cant. respectively. SAE and SE are in mils.

SE is part of the data in appendix A. T was set at 2 degrees for all fire control systems.

Reticle Error

It was decided that the mean range error, when using a reticle, was 20 m. The resulting angular error is then 20 dE/dR, where R is range in meters and E is superelevation in mils and dE/dR can be found in appendix A.

The method is the same as with range error.

Only systems 2 and 3 have reticle errors for only those systems have reticles. Reticle error is vertical.

Boresight, Fire Control Solution, Jump Dispersion, and Zeroing Error

All of these error sources are the same for all systems, all ranges, and both directions. The values assigned to boresight, fire control solution, jump dispersion, and zeroing error were 0.1 mil, 0.1 mil, 0.25 mil, and 0.3 mil, respectively.

Aiming Error

The vertical aiming error is based on 1/6th of the target's height. Similarly, the horizontal aiming error is based on 1/6th of the target's width. So if T is the appropriate target dimension and R is the range, then the aiming error is T/6R radians.

The target for the AP and SLAP rounds was a NATO vehicle target which is 2.3 m². The target for the other rounds was a rectangle 1 m high and 1.2 m wide which resembles the NATO personnel target.

Resolution

The value of 0.06 mil was used for the resolution error for all systems at all ranges and for both horizontal and vertical error.

Bullet Dispersion

The value of bullet dispersion is mils depends on the round and, in some cases, on direction. It is independent of system and range. These values were obtained from the appropriate ammunition authorities.

CONCLUSIONS

System 4 should be used with all weapons except the M21 and M24 sniper weapons for which it produces only a slight improvement over their present fire control systems.

REFERENCES

- 1. Cerrato, L. R. and Pfleger, K. R., "Multiple Round Hit Probabilities Associated with Combat Vehicle Fire Control Gun Systems," Report R-3001, Frankford Arsenal, PA, May 1971.
- 2. Pfleger, K. R. and Bibbero, R. J., "The Evaluation of Combat Vehicle Fire Control/Gunnery Systems," Report R-1937. Technical Analysis Group, Frankford Arsenal, PA, September 1969.

APPENDIX A TABLES OF PROBABILITY OF HIT

The seven tables that follow present probabilities of hit for every ammunition and fire control system and for every range from 200 m to 2000 m. All tables, except the last one, show the probability of at least one hit from five shots and from ten shots. The last ammunition is the 7.62 mm M118 National Match. This is used only in a sniper rifle so only single-shot hit probabilities have been calculated for it.

The NATO vehicle target, which is $2.3~\text{m}^2$, was assigned to the AP and SLAP rounds. The target for the other rounds was a rectangle, 1-m high and 1/2-m wide, which represents a crouching man. It is similar to the NATO personnel target.

The reader can see how the probability of hit decreases with increasing range and how it increases as the fire control system improves.

.50 CAL M8 API

	PROBAB	ILITY OF I	1 OR MORE	HITS	PROBAB		1 OR MORE SHOTS	HITS
RANGE (METERS)	SYS	SYS 2	SYS 3	SYS 4	SYS 1	SYS 2	SYS 3	SYS 4
200	1.	1.	1.	1.	1.	1.	1.	1.
400	.9992	.9996	.9998	.9999	1.	1.	1.	1.
600	.9365	.9611	.9789	.993	.9842	.9938	.9974	.9999
800	.667	.7492	.8538	.9462	.8059	.8805	.946	.995
1000	.3714	.4562	.6473	.8374	.5058	.6106	.799	.9615
1200	.1844	.2401	.4495	.6904	.2727	.3522	.6114	.8767
1400	.0893	.1198	.2935	.5409	.1399	.187	.4333	.7506
1600	.044	.0599	.1821	.4098	.072	.0979	.2871	.6109
1800	.023	.0315	.1125	.3083	.0388	.0532	.186	.4857
2000	.013	.0179	.0708	.2333	.0225	.031	.1211	.3836

.50 CAL M20 APIT

	PROBAB	LITY OF I		HITS	PROBAB		OR MORE	HITS
RANGE (METERS)	SYS 1	SYS 2	SYS 3	SYS 4	SYS 1	SYS 2	SYS 3	SYS 4
200 400 600 800 1000	1. .9992 .9355 .6596 .363	1. .9996 .9602 .7425 .4469	1. .9998 .9781 .8495 .6392 .4402	1. .9999 .9929 .9452 .834 .6845	1. 1. .9838 .7989 .4953 .2639	1. .9935 .8749 .5995	1. 1. .9972 .9429 .7907 .6001	1. 1. .9999 .9947 .9593 .8711
1400 1600 1800 2000	.0856 .042 .0218 .0001	.115 .0572 .0298 .0168	.2853 .1761 .1076 .0667	.5335 .4026 .3015 .2266	.1342 .0687 .0368 .0211	.1797 .0934 .0504 .0291	.422 .278 .1781 .1142	.7419 .6012 .4757 .3732

.50 CAL M33 BALL

PROBABILITY OF 1 OR MORE HITS
IN 5 SHOTS

PROBABILITY OF 1 OR MORE HITS
IN 10 SHOTS

RANGE (METERS)	SYS 1	SYS 2	SYS 3	SYS 4	SYS 1	SYS 2	SYS 3	SYS 4
200	1.	1.	1.	1.	1.	1.	1.	1.
400	.9997	.9999	1.	1.	1.	1.	1.	1.
600	.9453	.9692	.9847	.9969	.9849	.9944	.9975	1.
800	.6774	.7609	.8649	.9589	.8075	.8821	.9461	.9963
1000	.3784	.4648	.6575	.8535	.509	.6142	.8004	.9657
1200	.1888	.2455	.4572	.705	.2765	.3566	.6146	.8835
1400	.092	.1233	.2994	.552	.1432	.1912	.4381	.7584
1600	.0445	.0607	.1857	.4178	.0725	.0986	.2909	.6182
1800	.0232	.0318	.1136	.3131	.039	.0535	.187	.4908
2000	.0131	.018	.0709	.2358	.0226	.0311	.121	.3865

7.62 MM M80 BALL

	PROBABIL	ITY OF 1 (IN 5 SHO	OR MORE H	ITS	PROBAB		L OR MORE SHOTS	HITS
RANGE (METERS)	SYS 1	SYS 2	SYS 3	SYS 4	SYS 1	SYS 2	SYS 3	SYS 4
200	.9942	.9943	.9945	.9985	.9993	.9993	.9993	.9999
400	.6217	.6729	.7364	.8922	.7539	.8008	.8468	.9684
600	.1744	.2208	.3665	.6	.2528	.3174	.4992	.7748
800	.0417	.056	.149	.3356	.0665	.0892	.2309	.4987
1000	.0124	.017	.0583	.1816	.021	.0287	.0978	.2958
1200	.0046	.0063	.0251	.1018	.0081	.0112	.0442	.1757
1400	.002	.0027	.0118	.058	.0036	.005	.0214	.104
1600	.0009	.0013	.0059	.0331	.0017	.0024	.0108	.0608
1800	.0005	.0007	.003	.019	.0009	.0013	.0057	.0356
2000	.0003	.0004	.0016	.0109	.0005	.0007	.0031	.0207

7.62 MM SLAP XM948

	PROBAB	ILITY OF IN 5 S	-	HITS	PROBAB		1 OR MORE SHOTS	HITS
RANGE (METERS)	SYS 1	SYS 2	SYS 3	SYS 4	SYS 1	SYS 2	SYS 3	SYS 4
200	1.	1.	1.	1.	1.	1.	1.	1.
400	1.	1.	1.	1.	1.	1.	1.	1.
600	.9566	.9741	.9817	.9994	.9819	.9904	.9928	.9999
800	.5572	.6598	.807	.972	.6388	.7425	.8615	.9891
1000	.1917	.2529	.5146	.8302	.2349	.3081	.5869	.8889
1200	.0618	.084	.2537	.6106	.0783	.1063	.3105	.6907
1400	.0242	.0331	.1179	.4218	.0314	.043	.1509	.503
1600	.0105	.0144	.0564	.2736	.0139	.0191	.0743	.3438
1800	.0052	.0071	.0282	.167	.007	.0096	.038	.2195
2000	.0027	.0037	.0145	.0969	.0038	.0052	.02	.132

.50 CALIBER SLAP XM903

	PROBAB	ILITY OF IN 5 S		HITS	PROBAB		1 OR MORE SHOTS	HITS
RANGE								
(METERS)	SYS 1	SYS 2	SYS 3	SYS 4	SYS 1	SYS 2	SYS 3	SYS 4
200	1.	1.	1.	1.	1.	1.	1.	1.
400	1.	1.	1.	1.	1.	1.	1.	1.
600	.9986	.9996	.9999	1.	.9998	1.	1.	1.
800	.9572	.9826	.9953	.9992	.9824	.9956	.9993	1.
1000	.7974	.8825	.9638	.9934	.8701	.9405	.9875	.9993
1200	.572	.6871	.8834	.9747	.6652	.7837	.9407	.9951
1400	.376	.4787	.7636	.9356	.4605	.579	.8514	.9812
1600	.2375	.313	.6285	.8749	.3032	.3967	.7344	.9518
1800	.1482	.1994	.4974	.7962	.1958	.2624	.6087	.9036
2000	.0914	.1246	.3773	.7068	.1244	.1691	.4832	.8382

7.62 MM BALL M118 (MATCH)

SINGLE SHOT HIT PROBABABILITY PALNH(1)

RANGE				
(METERS)	SYS 1	SYS 2	SYS 3	SYS 4
100	.9842	.9841	.9842	.9856
200	.8819	.8842	.8878	.9259
300	.6005	.6236	.6512	.7825
400	.3073	.3495	.4204	.6028
500	.1401	.1731	.2614	.4397
600	.0638	.0829	.1617	.3125
700	.0298	.0399	.0989	.2197
800	.0147	.0199	.0595	.1539
1000	.0041	.0057	.0213	.0759
1200	.0015	.0021	.0087	.0399
1400	.0006	.0009	.004	.0217
1600	.0003	.0004	.002	.0122
1800	.0002	.0002	.0011	.007
2000	.0001	.0001	.0006	.0041

APPENDIX B

ERROR BUDGETS

If there is only one number in a column, then the horizontal and vertical components of the error are both equal to this number.

.50 CALIBER H20 APIT - SYSTEM 1

			•							
	200 H V	7 × 400	> N	> ×	E -000	1200 H V	1400 K	1600	1800 N	2000 E V
BANGE	0318	0743	0-1.313	021	0-3.134	0-4.582	0-6.533	0-9.081	0-12.194	0-15.556
CANT	.116-0	.258-0	.418-0	.613-0	.853-0	1.138-0	1.484-0	1.911-0	2.436-0	3.049-0
WIND	. 229-0	.477003	.756009	1.069018	1.421034	1.818061	2.264103	2.75617	3.24263	3.697382
VELOCITY	0031	0064	0107	016	0~.225	0306	6070	0535	0669	080\$
TEMPERATURE	0-0	0-0	0005	0013	0039	0052	0085	0118	0111	0056
DENBITY	0005	0024	0065	0138	0257	0444	073	0-1.115	0-1.544	0-2.011
EARTH RATE	600.	.019	160.	. 046	.063	.083	. 106	. 134	. 164	. 196
BITE ANGLE	0001	0003	0003	0004	9000	0008	001	0013	0017	0021
RETICLE	0	0	0	0	0	0	0	0	•	•
BORESIGHT	•	-	-		1.		1.		.1	-
8017110N	•	1.	-	٠.		-	•	.1	1.	-
JUMP DISPERSION	.25	.25	.25	.25	. 25	.25	.25	. 25	.25	.25
BEROIMG	.3		e.	6.	6	.3	.3	.3	6.	6.
AIMING	1.94-1.94	.9797	.647647	.485485	.388388	.323323	772772.	.243243	.216216	. 194 194
RESOLUTION	90.	91).	90.	90.	90.	90.	90.	90.	90.	90.
AMOUNITION DISPERION	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
BYSTEM	2.237-2.508 1.553-1.98	1.553-1.981	1.53-2.141	1.53-2.141 1.712-2.668 2.019-3.539	2.019-3.539	2.426-4.882 2.931-6.776	2.931-6.776	3.536-9.303	4.205-12.41	4.921-15.79
ROUND-TO-ROUND	2.183-2.453	1.394-1.787	1, 193-1,635	1.113-1.578	1.113-1.578 1.074-1.551	1.053-1.536	1.053-1.536 1.039-1.527 1.031-1.521 1.025-1.517	1.031-1.521	1.025-1.517	1.02-1.514
OCCASION-TO- OCCASION	.488524	.603854	.959-1.383	.959-1.383 1.301-2.151		1.71-3.181 2.186-4.634 2.741-6.602 3.382-9.178 4.078-12.32 4.814-15.72	2.741-6.602	3.382-9.178	4.078-12.32	4.814-15.72

.50 CALIBER M20 APIT - SYSTEM 2

	200 H V	7 × ×	009 E A	800 H V	1000 H V	1200 H V	1400 H V	1600 H V	1600 V	2000 EE V
RANGE	0227	0531	0938	0-1.5	0-2.239	0-3.273	0-4.667	0-6.486	0-8.71	0-11.111
CANT	.116-0	.258-0	.418-0	.613-0	.853-0	1.138-0	1.484-0	1.911-0	2.436-0	3.049-0
ONIA	.229-0	.447003	.756009	1.069018	1.421034	1.818061	2.264103	2.75617	3.24263	3.697382
VELOCITY	0031	0064	0107	016	0225	0306	0409	0535	0669	0805
TEMPERATURE	0-0	0-0	0005	0013	0029	0052	0085	0118	0111	0056
DENBITY	0005	0024	0065	0138	0257	0444	073	0-1.115	0-1.544	0-2.011
EARTH RATE	600.	.019	.031	.046	.063	.083	. 106	134	.164	. 196
SITE ANGLE	0001	0005	0003	0004	9000	0008	001	0013	0017	0031
RETICLE	0152	0177	0208	025	0299	0364	0444	0541	0645	0741
BORESIGHT	1.		.1			-	.1		•	
HOILINIOS 2		1.	•	• 1	•	•1	• 1		.1	
NOISPERSION	.25	.25	.25	.25	.25	.25	. 25	.25	.25	.25
SEROING		.3	.3	.3	.3	.3	.3	.3	ť.	e.
									-	
ALMINO	1.24-1.34	/s/s-	199'-/99'	.485685	.388388	.323323	.277277	.243243	.216216	194194
· RESOLUTION	90.	90.	90.	90.	90.	90.	90.	90.	90.	90.
AMMUNITION DISPERION	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
SYSTEM	2.237-2.503 1.553-1.92	1.553-1.92	1.53-1.945	1.712-2.241 2.019-2.793	2.019-2.793	2.427-3.699	2,931-5.021	2.427-3.699 2.931-5.021 3.536-6.814 4.205-9.038 4.921-11.46	4.205-9.038	4.921-11.46
BOUND-TO-ROUND	2.183-2.453 1.394-1.78	1.394-1.787	1.193-1.635	1.113-1.578	1.074-1.551	1.053-1.536	1.039-1.527	1.113-1.576 1.074-1.551 1.053-1.536 1.039-1.527 1.031-1.521 1.025-1.517	1.025-1.517	1.02-1.514
OCCASION-TO- OCCASION	.488498	.683701	.959-1.055	.959-1.055 1.301-1.591	1.71-2.323	2.186-3.365	2.741-4.783	1.71-2.323 2.186-3.365 2.741-4.783 3.382-6.643 4.078-8.91 4.814-11.36	4.078-8.91	4.814-11.36

.50 CALIBER M20 APIT - SYSTEM 3

	200 H V	7 7 9 9	600 H	800 H V	1000 H ×	1200 H V	1400 M	1600 H V	1800 N	2000 M V
RANGE	0076	0089	0104	0125	0149	0182	0222	027	0323	037
CMT	.116-0	.258-0	.418-0	.613-0	.853-0	1.138-0	1.484-0	1.911-0	2.436-0	3.049-0
MIND	. 229-0	.477003	.756009	1.069018	1.421034	1.818061	2.264103	2.75617	3.24263	3.697382
VEOCITY	0031	₹900	0107	016	0225	0306	0409	0535	699*-0	0805
TIMPERATURE	0-0	00	0005	0013	0039	0052	0085	0118	0111	0056
DENSITY	0005	0024	0065	0138	0257	0444	073	0-1.115	0-1.544	0-2.011
EARTH RATE	600.	.019	160.	.046	.063	.083	. 106	.134	. 164	196
BITE ANGLE	100.	.002	.003	♦00 .	900.	B00.	.01	.013	.017	.021
RETICLE	0152	0177	0208	025	0299	0364	0444	0541	0645	0741
BORESIGHT	-	1.	-	-	-		•	-	.1	-
S BOLLTION		•			.1	.1	.1	-	• 1	.1
O JUMP DIBPERSION	.25	.25	.25	.25	.25	.25	.25	.25	.25	.25
SEROING	.3	.3	.3	.3	.3	.3	.3	e.	.3	6.
AIMING	1.94-1.94	7676.	.647647	. 485 485	.388388	.323323	772772	.243243	.216216	. 194 194
RESOLUTION	90.	90.	90.	90.	90.	90.	90.	90.	90.	90.
AMUNITION DISPERION	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
BYBTEM	2.237-2.494 1.553-1.84	1.553-1.847		1.53-1.707 1.712-1.669	2.019-1.677		2.931-1.865	2.426-1.732 2.931-1.865 3.536-2.107	4.205-2.436 4.921-2.834	4.921-2.834
ROUND-TO-ROUND	2.183-2.453 1.394-1.76	1.394-1.787	1.193-1.635	1.113-1.578	1.074-1.551	1.053-1.536	1.039-1.527	87 1.193-1.635 1.113-1.578 1.074-1.551 1.053-1.536 1.039-1.527 1.031-1.521 1.025-1.517	1.025-1.517	1.02-1.514
OCCABION-TO- OCCABION	.48845	.683465	.959-493	1.301546	1.71638	2.186801	2.741-1.072	2.186801 2.741-1.072 3.382-1.459 4.078-1.906 4.814-2.396	4.078-1.906	4.814-2.396

.50 CALIBER M20 APIT - SYSTEM 4

200 H V 0076	9 7	600 H V 0104 .042-0	800 H V 0125 .061-0	1000 H V O O - 149	1200 B V 0182 .114-0	1400 B V 0222 .148-0	1600 <u>H</u> V 027 .191-0	1800 W V 0323 .244-0 1.693263	2000 H V O37 .305-0
	0-0	0021	0032	0045	001	0082	0107	0134	0011
.009	0005	0013	0028	0051	0089	0146	0223	0309	0402
0001	0002	0003	0004	9000	0008	001	0013	0017	0021
11		-					1.		
- 1	1.	1.		1.	1.	1.	••	1.	1.
i	.25	.25	.25	.25	.25	.25	.25	.25	.25
	.3	6.	6.	.3	.3	.3	.3		Ę.
1.94-1.94	.9797	.647647	.485485	.388388	.323323	.277277	.243243	.216216	. 194 194
i	90.	90.	90.	90.	90.	90.	90.	90.	90.
	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
21	2.226-2.489 1.477-1.837	1.324-1.69	1.315-1.637	1.374-1.615	1.484-1.608	1.374-1.615 1.484-1.608 1.639-1.613 1.834-1.633 2.043-1.669 2.253-1.724	1.834-1.633	2.043-1.669	2.253-1.724
- 1	2.183-2.453 1.394-1.787	1.193-1.635 1.113-1.578		1.074-1.551 1.053-1.536	1.053-1.536	1.039-1.527 1.031-1.521 1.025-1.517	1.031-1.521	1.025-1.517	1.02-1.514
.433422	.485425	.57643	.7439	.857452	1.046478	1.267522	1.517595	1.768698	2.008826

.50 CALIBER 10 API - SYSTEM 1

	200 M V	× 400	V 2	6000 M	1000 H V	1200 H V	1400 V	1600 V	1800 W W	2000 E
PANGE	0318	0743	0-1.313	0-2.074	03088	0-4.5	0-6.391	0-8.842	0-11.013	0-15.
CANT	.116-0	.258-0	.418-0	.614-0	.846-0	1.121-0	1.46-0	1.878-0	2.385-0	2.973-0
MIND	. 224-0	.467003	.74008	1.043017	1.382031	1.764056	2.196095	2.679157	3.15244	3.585355
VILOCITY	0031	0~.064	0107	0158	0221	03	0399	0523	0655	0783
TEMPERATURE	0-0	0003	9000	0017	0032	0055	1600	0131	0126	007
DENGITY	0~.005	0024	0064	0133	0246	0424	0698	0-1.074	0-1.476	0-1.901
EARTH RATE	600.	610.	.031	.045	.062	.082	. 105	. 132	.161	. 192
BITE ANGLE	0001	0003	0003	0004	9000	0008	100	0013	0016	002
RITICIE	0	0	0	0	0	0	0	•	0	0
BORESIGHT	-	-	-		١.	-		-	-	
SOLUTION		1.	.1		.1	1.	-	•	•	••
JUNP DISPERSION	.25	.25	.25	.25	.25	.25	.25	.25	.25	.25
BROING	.3	.3	.3	ε.	.3	.3	€.	6.	€*	.3
AINING	1.94-1.94	7676.	.647647	. 485 485	.388388	.323323	.277277	.243243	.216216	. 194 194
RESOLUTION	90.	90.	90.	90.	90.	90.	90.	90.	90.	90.
AMMUNITION DISPERION	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
BYSTEM	2.237-2.508	1.55-1.981	1.522-2.141	1.697-2.647	1.989-3.497	2.378-4.802		2.867-6.635 3.458-9.064	4.106-12.03	4.79-15.227
ROUND - TO - ROUND	2.183-2.453 1.394-1.76	1.394-1.787	1.193-1.635	1.113-1.578	1.074-1.551	37 1.193-1.635 1.113-1.578 1.074-1.551 1.053-1.536	1.039-1.527	1.039-1.527 1.031-1.521 1.025-1.517	1.025-1.517	1.02-1.514
OCCABION-TO- OCCABION	.486-,524	.676854	.946-1.383		1.674-3.134	2.132-4.55	2.672-6.457	1.28-2,126 1.674-3,134 2.132-4.55 2.672-6.457 3.301-8.935 3.976-11.93 4.68-15.151	3.976-11.93	4.68-15.151

.50 CALIBER MO API - SYSTEM 2

		200 H V	00 7	009 N	008 N	1000 N	1200 H V	1400 K	1600 H	1800 V	2000 B V
PANGE		0227	0531	0938	0-1.481	0-2.206		0-4.565		0-8.438	0-10.714
CLNT		.116-0	.258-0	.418-0	.614-0	.846-0	1.121-0	1.46-0	1.878-0	2.385-0	2.973-0
Q IN		.224-0	.467003	.74008	1.043017	1.382031	1.764~.056	2.196095	2.679157	3.15244	3.585355
VELOCITY	ī	0031	0064	0107	0158	0221	03	0399	0523	0655	0783
TEMPERATURE	ATURE	0-0	0003	0008	0017	0032	0~.055	0091	0131	0126	007
DENBITY	>	0005	0024	0064	0133	0246	0424	0698	0-1.074	0-1.476	0-1.901
KARTH BATE	RATE	600.	.019	.031	.045	.062	.082	.105	. 132	.161	. 192
BITE ANGLE	NGI.	0001	0003	0003	0004	900'-0	0~.008	001	0013	9016	003
RETICLE	H	0152	0177	0208	0247	0294	0357	0435	0526	0625	0714
BOREGIGHT	GHT		.1	.1		• 1	•1	.1	•	•1	•
Sourrios	75	.,	.1	• 1	.1	• 1	.1	1.	.1	.1	1.
a ating	JUMP DISPERSION	.25	.25	.25	. 25	.25	.25	.25	.25	.25	.25
SHIONER	U	е.	.3	E.	.3	.3	.3	.3	e.	.3	.3
AIMING		1.94-1.94	.9797	.647647	.485485	.388388	.323323	רוברוב.	.243243	.216216	. 194 194
RESOLUTION	TION	90.	90.	90.	.06	90.	90.	.06	90.	90.	90.
APPUNITION DISPERSON	TION	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
BYSTEM	_	2.237-2.503	1.55-1.92	1.522-1.945	1.522-1.945 1.697-2.227	1.989-2.765	2.3	2.867-4.92	3.458-6.644	3.458-6.644 4.106-8.762 4.79-11.053	4.79-11.053
-GUND-	ROUND-TO-ROUND	2.163-2.453 1.394-1.7		1.193-1.635	1.113-1.578	1.074-1.551	1.053-1.536	1.039-1.527	87 1.193-1.635 1.113-1.578 1.074-1.551 1.053-1.536 1.039-1.527 1.031-1.521 1.025-1.517	1.025-1.517	1.02-1.514
OCCABION OCCABION	OCCASION-TO- OCCASION	.486498	.676701	.946-1.055		1.674-2.289	2.132-3.303	2.672-4.677	1.28-1.572 1.674-2.289 2.132-3.303 2.672-4.677 3.301-6.467 3.976-8.63 4.68-10.948	3.976-8.63	4.68-10.948

.50 CALIBER NO API - SYSTEM 3

	200 H V	400 V	600 V	900 N	1000 V	1200 H V	1400	1600 V	1800 1800	2000 H V
RANGE	0076	0~.088	0104	0123	0147	0179	017	0263	0313	0357
CANT	. 116-0	.258-0	.418-0	:614-0	.846-0	1.121-0	1.46-0	1.878-0	2.305-0	2.973-0
QHIM	.224-0	.467003	.74008	1.043017	1.382031	1.764056	2.196095	2.679157	3.15244	3.585355
VELOCITY	0031	0064	0107	0158	0221	03	0399	0523	0655	0783
TEMPERATURE	0-0	0003	9000	0017	0032	0055	0091	0131	0126	007
DENBITY	0005	0024	0064	0133	0246	0424	0698	0-1.074	0-1.476	0-1.901
EARTH RATE	600.	.019	160.	.045	.062	.082	. 105	. 132	. 161	. 192
BITE ANGLE	0001	0003	0003	0004	9000	0008	001	0013	9016	002
REFICIA	0152	0177	0208	0247	0294	0357	0435	0526	0625	0714
BORESIGHT	-	-	•	-	. 1	.1	.1		••	
SOLUTION Q	-	٠.	-	-	-			•	-	
JUMP DIBPERSION	.25	.25	.25	.25	.25	.25	.25	.25	.25	.25
RENOING	.3	.3	.3	.3	6.	.3	.3	е.		e.
AIMING	1.94-1.94	.9797	.647647	.485485	.388388	.323323	.277277	.243243	.216216	194194
RESOLUTION	90.	90.	90.	90.	90.	90.	90.	90.	90.	90.
AMBURITION	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
BYSTEM	2.237-2.494	1.55-1.847	1.522-1.707	1.697-1.668	1.989-1.673	2.378-1.724	2.867-1.848	3.458-2.078	4.106-2.381	4.79-2.738
ROUND-TO-ROUND	2.183-2.453 1.394-1.	1.394-1.787	787 1.193-1.635	1.113-1.578	1.074-1.551	1.113-1.578 1.074-1.551 1.053-1.536 1.039-1.527	1.039-1.527	1.031-1.521	1.031-1.521 1.025-2.517	1.02-1.514
OCCASION-TO- OCCASION	.48645	.676465	.946493	1.28542	1.674629	2.132784	2.672-1.041 3.301-1.416 3.976-1.836	3.301-1.416	3.976-1.836	4.68-2.281

.50 CALIBER MS API - SYSTEM 4

	200 H V	7 P	9 P	900 H	1000 H V	1200 H V	1400 H V	1600 M V	1600 H V	2000 E
RANGE	0076	0088	0104	0123	0147	0179	0217	0263	0313	0357
CANT	.012-0	.026-0	.042-0	.061-0	.085-0	.112-0	. 146-0	.188-0	.239-0	.297-0
CNIA	.117-0	.244003	.387008	.545017	.722031	.921056	1.147095	1.399157	1.645244	1.873355
VELOCITY	9000	0013	0021	0032	0044	900	900	0105	0131	0157
TEMPERATURE	0-0	0001	0003	0003	9000	0011	0018	0026	0025	0014
DENSITY	0001	0005	0013	0027	0049	0085	014	0215	0295	038
EARTH RATE	600.	.019	160.	.045	.062	.082	. 105	. 132	. 161	. 192
BITE ANGLE	0001	0002	0003	0004	9000	0008	001	0013	0016	002
RETICLE	0	0	0.	0	0	0	0	0	0	0
BORESIGHT	•	-	-			-	-	-		-
BOLUTION		•	1.	.1	•		•	1	•1	-
JUMP DISPERSION	. 25	.25	.25	.25	.25	.25	.25	.25	.25	.25
EROING	.3	.3	6.	.3	E.	e.	.3	.3	E,	
AINING	1.94-1.94	.9797	.647647	.485485	. 388 388	.323323	772772.	.243243	.216216	. 194 194
RESOLUTION	90.	90.	90.	90.	90.	90.	90.	.06	.06	90.
AMMUNITION DISPERSON	11.5	11.5	11.5	11.5	1,-1.5	11.5	11.5	11.5	11.5	11.5
SYSTEM	2.226-2.489	2.226-2.489 1.476-1.837	1.322-1.69	1.309-1.637	1.363-1.615 1.466-1.607 1.613-1.611 1.801-1.629 2.003-1.662 2.202-1.71	1.466-1.607	1.613-1.611	1.801-1.629	2.003-1.662	2.202-1.71
ROUND-TO-ROUND	2.183-2.453	2.183-2.453 1.394-1.787 1.193-1.635 1.113-1.578	1.193-1.635	1.113-1.578		1.053-1.536	1.074-1.551 1.053-1.536 1.039-1.527 1.031-1.521 1.025-1.517	1.031-1.521	1.025-1.517	1.02-1.514
OCCABION-TO- OCCABION	.432422	.483425	.5743	.689438	.839451	1.02475	1.233516	1.477585	1.721679	1.951795

.50 CALIBER M33 BALL - SYSTEM 1

		200	, ,	909	008	1000	1200	1400	1600	1600	2000
					21		91				
	PANGE	0316	0737	0-1.299	0-2.049	0-3.043	0-4.421	0-6.255	0-8.842	0-11.813	0-15.
	CLUT	.116-0	.258-0	.418-0	.604-0	.836-0	1,111-0	1.44-0	1.649-0	2.356-0	2.933-0
	QNIN	:217-0	.456003	.722007	.722007 1.019015	1.352029	1.728053	2.15509	2.63215	3.111235	3.558345
	VELOCITY	0031	0064	0107	0158	0222	0301	0403	0526	0664	0801
	TEMPERATURE	0-0	0004	6000	002	0037	0063	0103	0151	0164	0126
	DENSITY	0005	0024	0062	0129	024	0414	0682	0-1.057	0-1.477	0-1.923
	EARTH RATE	600.	.019	.031	.045	.06.	.081	. 104	.131	.161	. 192
	SITE ANGLE	0001	0002	0003	0004	0~.006	9000	001	0013	0016)03
	BETICLE	0	0	0	0	0	0	0	0	•	•
	BORESIGHT		1.	1.	1.		.1	1.	1.	.1	
3	ROLLTION	-	-			-		. 1	• 1	.1	
34	JUMP DISPERSION	.25	.25	. 25	.25	.25	.25	.25	.25	.25	.25
	ZEROING	.3	.3	.3	.3	.3	.3	6.	.3	.3	.3
	AIMING	.424849	.212424	.141283	. 106212	.08517	.071141	.061121	.053106	.047094	.042085
	RESOLUTION	90.	90.	90.	90.	90.	90.	90.	90.	90.	90.
	AMMUNITION	1,-1.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
	BYSTEM	1.19-1.802	1.223-1.776	1.19-1.802 1.223-1.776 1.376-2.052	1.61-2.591	1.61-2.591 1.927-3.44	2.326-4.719	2.326-4.719 2.812-6.498 3.397-9.06		4.054-12.03 4.741-15.23	4.741-15.23
	ROUND-TO-ROUND	1.088-1.725	1.088-1.725 1.024-1.56	1.012-1.528	1.007-1.516	1.005-1.511	1.012-1.528 1.007-1.516 1.005-1.511 1.004-1.508 1.004-1.506 1.003-1.505 1.003-1.504 1.003-1.504	1.004-1.506	1.003-1.505	1.003-1.504	1.003-1.504
	OCCASION-TO-	.483523	.669849	.932-1.37	1.256-2.101 1.644-3.09		2.097-4.471 2.627-6.321 3.246-8.934 3.928-11.94 4.634-15.16	2.627-6.321	3.246-8.934	3.928-11.94	4.634-15.16

.50 CALIBER M33 BALL - SYSTEM 2

		200 M	7 P	N 600	800 H V	1000 H V	1200 H V	1400 E V	1600 H V	1800 N M	2000 H V
	BANGE	0226	0526	0928	0-1.463	0-2.174	0-3.158	0-4.468	0-6.316	0-0.438	0-10.714
-	CLUIT	.116-0	.258-0	.418-0	.604-0	.836-0	1.111-0	1.44-0	1.849-0	2.356-0	2.933-0
	MIMD	.217-0	.456003	.722007	1.019015	1.352029	1.728053	2.15509	2.63215	3,111-,235	3.558345
-	VILOCITY	0031	0064	0107	0158	0222	0301	0402	0526	0664	0801
	TEMPERATURE	0-0	0004	6000	003	0037	0063	0103	0151	0164	0126
_	DENGITY	0005	0024	0062	0129	024	0414	0682	0-1.057	0-1.477	0-1.923
	EARTH RATE	600.	.019	.031	.045	.062	180.	104	181.	.161	. 192
-	BITE ANGLE	0001	0005	0003	9000	9000	0008	100	0013	0016	002
	RETICLE	015	0175	0206	0244	029	0351	0426	0526	0625	0714
	BORESIGHT	-	-	-	•	.1	.1	.1	.1	.1	.1
	BOLUTION	-	•	-	•1	•1		.1	1.		1.
35	JUMP DISPERSION	.25	.25	.25	.25	.25	.25	.25	.25	.25	. 25
	ZEROING	.3	.3	.3	.3	.3	.3	.3	E,	.3	.3
_	AIMING	.424849	.212424	.141283	.106212	.085170	.071141	.061121	.053106	.047094	.042085
-	RESOLUTION	90.	90.	90.	90.	90.	90.	90.	90.	90.	90.
•	AMMINITION DISPERSION	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
_	BYSTEM	1.19-1.795 1.223-1.	1.223-1.708	1.376-1.851	1.61-2.172	1.927-2.716	2.326-3.58	2.612-4.621	3.397-6.638	4.054-8.761	4.741-11.06
	ROUND-TO-ROUND	1.088-1.725 1.024-1.	و	1.012-1.528	1.012-1.528 1.007-1.516 1.005-1.511 1.004-1.508 1,004-1.506 1.003-1.505 1.003-1.504 1.003-1.504	1.005-1.511	1.004-1.508	1,004-1.506	1.003-1.505	1.003-1.504	1.003-1.504
	OCCASION-TO- OCCASION	.483497	969699.	.932-1.045	.932-1.045 1.256-1.555 1.644-2.257 2.097-3.247 2.627-4.58	1.644-2.257	2.097-3.247	2.627-4.58	3.246-6.465 3.928-8.631 4.634-10.95	3.928-8.631	4.634-10.95

.50 CALIBER M33 BALL - SYSTEM 3

		200 M V	400 ×	009 M	008 R	1000 H	1200 H V	1400	1600 H	1800 V	2000 M
- •	RANGE	0075	0089	0103	0122	0145	0175	0213	0263	0313	0357
•	CANT	.116-0	.258-0	.418-0	.604-0	.836-0	1.111-0	1.44-0	1.849-0	2.356-0	2.933-0
	WIND	.217-0	.456003	.722007	1.019015	1.352029	1.728053	2.15509	2.63215	3.111235	3,558345
_	VELOCITY	0031	0064	0107	0158	0223	0301	0402	0526	0664	0801
••	TEMPERATURE	0-0	0004	6000	002	0037	0063	0103	0151	0164	0126
	DENSITY	0005	0024	0062	0129	024	0414	0682	0-1.057	0-1.477	0-1.923
-	EARTH RATE	600.	.019	.031	.045	.062	.081	104	.131	. 161	. 192
-	SITE ANGLE	1000	0003	. 0003	₽000	900'-0	0008	100	0013	0016	002
-	RETICLE	015	0175	0206	0244	029	0351	0426	0526	0625	0714
-	BORESIGHT	-	١.		-		-	-	•	.1	•
3	BOLUTION	-				.1	-	+	.1	•	•
-	JUMP DISPERSION	.25	.25	.25	. 25	.25	.25	.25	.25	.25	.25
	ZERDING	.3	.3	.3	.3	.3	.3	.3	.3	.3	
	AIMING	.424849	.212424	.141283	.106212	.08517	.071141	.061121	.053106	.047094	.042085
-	RESOLUTION	90.	90.	90.	90.	90.	90.	90.	90.	90.	90.
	AMMUNITION	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	1,-1.5
-	BYSTEM	1.19-1.782	1.19-1.782 1.223-1.628	1.376-1.605		1.61-1.609 1.927-1.635		2.326-1.695 2.812-1.823 3.397-2.059 4.054-2.387 4.741-2.754	3.397-2.059	4.054-2.387	4.741-2.754
	ROUND-TO-ROUND	1.088-1.725 1.024-1.56	1.024-1.56	1.012-1.528	1.007-1.516	1.012-1.528 1.007-1.516 1.005-1.511	1.004-1.508	1.004-1.508 1.004-1.506	1.003-1.505	1.003-1.504 1.003-1.504	1.003-1.504
	OCCABION-TO- OCCABION	. 483 449	.669465	.932492	1.25654	1.644625	2.097775	2.627-1.027	3.246-1.405 3.928-1.842 4.634-2.307	3.928-1.842	4.634-2.307

.50 CALIBER M33 BALL - SYSTEM 4

PANGE	H V 0075	N N N N N N N N N N N N N N N N N N N	M V 0103	H V 0122	N N N N N N N N N N N N N N N N N N N	M V 0175	M V 0213	н V	N N N N N N N N N N N N N N N N N N N	N V N
	.012-0	.026-0	.042-0	0-90.	.084-0	.111-0	. 144-0	. 185-0	.236-0	.293-0
	. 113-0	.238003	.377007	.532015	.706029	.903053	1.12609	1,37515	1.625235	1.859345
VELOCITY	0006	0013	0021	0032	0044	900	008	0105	0133	016
TEMPERATURE	0-0	0001	0003	0004	0007	0013	0021	003	0033	0025
DENBITY	1000	0005	0012	0026	0048	0083	0136	0211	0295	0385
BARTH RATE	600.	.019	.031	.045	.062	180.	. 104	151.	. 161	. 192
BITE ANGLE	0001	0003	0~.003	000€	9000	000	001	0013	9100	003
RETICLE	0	0	0	0	0	0	0	0	0	0
BORESIGHT	-	-		-	-	٠.		-	.1	
BOLUTION	-	1.		-	.1	.1	.1			-
JUMP DISPERSION	.25	.25	. 25	.25	.25	.25	.25	.25	.25	.25
SKROING		e,	.3	.3	.3	.3	.3	.3	e.	E.
AIMING	.424849	.212424	.141283	. 106212	.08517	.071141	.061121	.053106	.047094	.042085
RESOLUTION	90.	.06	90.	90.	90.	90.	90.	90`	90.	90.
A-MUNITION DISPERION	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
BYSTEM	1.17-1.775	1.131-1.617	1.158-1.587	1.215-1.578	1.301-1.577	1.42-1.58	1.574-1.591	1.767-1.613	1.975-1.649	2.181-1.7
ROUND-TO-ROUND	1.088-1.725 1.024-1.56	1.024-1.56	1.012-1.528	1.007-1.516	1.005-1.511	1.004-1.508	1.004-1.508 1.004-1.506	1.003-1.505	1.003-1.505 1.003-1.504 1.003-1.504	1.003-1.504
OCCASION-TO- OCCASION	.431422	.48425	.56343	679- 437	37 - 360	1 003- 473	1 213- 612		1 701- 677	1.917794

.50 CALIBER GLAP XH903 - SYSTEM 1

	200 H V	700 x	P 200	N 800	1000 1000	1200 H V	1400 N	1600 H V	1900 K	2000 H V
RANGE	0165	0356	0581	0848	0-1.16	0-1.537	0-1.986	0-2.526	0-3.176	0~4.
CANT	.062-0	. 133-0	.204-0	.293-0	.382-0	0-84.	.587-0	.711-0	.844-0	0-966-
MIND	.084-0	. 173-0	.27001	.374002	.487003	.611-,005	.745008	.891012	1.052018	1.23026
VIELOCITY	001	0025	0041	0057	9200	6600	0124	0154	0189	0229
TEMPERATURE	0-0	0003	9000	0012	003	0032	0048	0069	0097	0134
DENSITY	0003	9000	0015	003	0052	0~.084	0128	0189	0271	0383
EARTH RATE	.003	.007	.01	.015	.019	.024	.029	.035	.042	50.
SITE ANGLE	0-0	1000	0001	0003	0003	0003	0004	0005	9000	1000
RETICLE	0	0	0	0	0	0	0	0	0	0
BORESIGHT	1.			.1	,	.1	• 1	•1	•	.1
BOLLTION			.1	.1	1.	1.	.1	.1	1.	1.
O JUMP DISPERSION	.25	.25	.25	. 25	.25	.25	.25	.25	.25	. 25
ZEROING		.3	.3	.3	6.	.3	.3	E.	£.	6.
AIMING	1.94	.97	.647	.485	.388	.323	772.	.243	.216	. 194
RESOLUTION	90.	90.	90.	90.	90.	90.	90.	90.	90.	90.
APPUNITION DISPERION	s.	.5	.5	.5	ı.	.5	s.	\$.	s.	\$:
BYSTEM	2.05-2.054	1.19-1.223	.979-1.088	.942-1.177	.98-1.39	1.065-1.706	1.184-2.117	1.336-2.633	1.514-3.268	1.724-4.085
ROUND-TO-ROUND	2.005	1.093	.82	669.	.636	. 598	\$78.	. 559	.548	. 539
OCCABION-TO- OCCABION	.428447	.469548	.536716	.631947	.746-1.236	.881-1.598	.881-1.598 1.036-2.038 1.214-2.573 1.412-3.222 1.637-4.049	1.214-2.573	1.412-3.222	1.637-4.049

.50 CALIBER GLAP XH903 - SYSTEM 2

	200 H V))	009 m	900 H	1000 V	1200 H V	1400 V	1600 V	1800	2000 H V
RANGE	0118	0254	0415	9090	0829	0-1.098	0-1.419	0-1.805	0-2.269	0-2.657
CANT	.062-0	. 133-0	.204-0	.293-0	.382-0	0-84.	.587-0	.711-0	. 844-0	0-966.
Quin	. 084-0	. 173-0	.27001	.374002	.487003	.611005	.745008	.891012	1.052018	1.23026
VELOCITY	001	0025	0041	0057	9200	6600	0124	0154	0189	0229
TEMPERATURE	0-0	0003	9000	0012	002	0032	0048	6900	7600	0134
DENEITY	0003	9000	0015	0~.03	0052	0084	0128	0189	0271	0383
EARTH RATE	.003	.007	10.	.015	.019	.024	.029	.035	.042	50.
BITE ANGLE	0-0	0001	1000	0003	0003	0003	₽20.~0	0005	9000	0007
RETICLE	0078	0085	0092	0101	011	0122	0135	015	0168	019
BORESIGHT		••			•	-	•	1.		
WOITTION O	•	• 1	1.		1.		•	• 1	.1	
JUMP DISPERSION	.25	.25	.25	.25	.25	.25	.25	.25	.25	.25
ERROING		.3	.3	.3	6.	.3	.3	.3	.3	e.
AIMING	1.94	.97	.647	.485	. 388	.323	772.	.243	.216	194
RESOLUTION	90.	90.	90.	90.	90.	90.	90.	90.	90.	90.
AMMUNITION	s.	5.	ĸĢ	s.	S.	S.	s.	s.	S	5.
BYETEM	2.05-2.052	1.19-1.2	.979-1.013	.942-1.021	.98-1.134	1.065-1.33	1.184-1.603	1.336-1.957	1.514-2.402	1.724-2.98
ROUND-TO-ROUND	2.005	1.093	.82	669.	.636	. 598	.574	. 559	.548	.539
OCCABION-TO- OCCABION	.428439	.469495	. 536 596	.631744	.746939	.881-1.188	1.036-1.496	1.214-1.876	.881-1.188 1.036-1.496 1.214-1.876 1.412-2.339 1.637-2.931	1.637-2.931

.50 CALIBER SLAP 20903 - SYSTEM 3

		200 H V	F 400	O P	B00	1000 E	1200 H V	1400 H V	1600 V	1000 M	2000 M
	FLAKCE	0039	0042	0046	0051	0055	0061	0068	0075	0084	0095
	CANT	.062-0	. 133-0	.204-0	.293-0	.382-0	.48-0	.587-0	.711-0	.844-0	0-966.
	MIND	.084-0	. 173-0	.27001	.374002	.487003	.611005	.745008	.891012	1.052010	1.23026
	VELOCITY	001	0025	0041	0057	0076	6600	0124	0154	0189	0239
	TEMPERATURE	0-0	0003	9000	0012	002	0032	0048	0069	0097	0134
	DENSITY	0003	9000	0015	003	0052	0084	0128	0189	0271	0383
	EARTH PATE	.003	.000	10.	.015	.019	.024	.029	.035	.042	.05
	BITE ANGLE	0-0	1000	0001	0003	0003	0003	0004	0005	9000	0007
	PATICIE	0078	0085	0092	0101	011	0122	0135	015	0168	019
	BORESIGHT	•	. 1	.,	.1	•-	.1	.1	.1	•1	1.
4	BOLUTION	-	-	1.	-	1.			-	-	-
0	JUMP DISPERSION	.25	.25	.25	.25	.25	.25	.25	.25	.25	.25
	REBOING	.3	.3	.3	.3	.3	.3	.3	.3	.3	C.
	AIMING	1.94	.97	.647	.485	.388	. 323	772.	.243	.216	194
	RESOLUTION	90.	90.	90.	90.	90.	90.	90.	90.	90.	90.
	AMUNITION	s.	s.	'n	ĸ.	s:	ĸį	s.	κį	s.	s:
	BYSTEM	2.05-2.049	1.19 1.173	.979926	.942842	.98775	1.065754	1.184748	1.33676	1.514792	1.724854
	ROUND-TO-ROUND	2.005	1.093	. 62	669.	.636	665,	.574	.559	.548	. 539
	OCCASION-TO-	.428424	.469427	.53643	.631436	.746444	.881458 1.03648	i	1.214516 1.412573 1.637662	1.412573	1.637662

.50 CALIBER SLAP XN903 - SYSTEM 4

		200 H V	400 H 4	600 EE <	800 H V	1000 V	1200 H V	1400 H V	1600 H V	1800 M	2000 H V
	PANGE	0039	0042	0046	0051	0055	0061	0068	0075	0084	0095
	CANT	0-900	.013-0	.02-0	.029-0	.038-0	.048-0	0-650.	.071-0	.084-0	.1-0
	GNIA	. 044-0	0-60.	. 141001	. 195002	.255003	.319005	.389008	.466012	.55018	.642026
	VELOCITY	0003	0005	0008	0011	0015	002	0025	0031	0038	0046
	TEMPERATURE	0-0	1000	0001	0002	0004	9000	001	0014	0019	0027
	DENSITY	0001	0001	0003	9000	001	0017	0026	0038	0054	0077
	EARTH RATE	.003	.007	.01	.015	.019	.024	.029	.035	.042	50.
	BITE ANGLE	0-0	0001	0001	0003	0003	0003	0004	0005	9000	0001
	RETICLE	9	0	0	0	0	0	0	0	•	0
	BORESIGHT		••	.1	.1	1.	.1	•1	.1	.1	.1
4	ROLLTION	•1	.1	••	.1		.1	•	.1	.1	.1
1	JUMP DISPERSION	.25	.25	.25	.25	.25	.25	.25	.25	.25	.25
	BEROING	.3	e.	.3	.3	.3	.3	.3	.3	.3	.3
	AIMING	1.94	.97	.647	.485	.388	.323	772.	.243	.216	194
	RESOLUTION	90.	90.	90.	90.	90.	90.	90.	90.	90.	90.
•	AMUNITION DISPERION	S,	s.	'n	ĸ,	ń	S	s.	e.	•	æ.
	SYSTEM	2.048-2.048 1.173-1.	1.173-1.17	.9392	.837815	.802762	267797.	.811714	.841703	.885697	.942696
	ROUND-TO-ROUND	2.005	1.093	.82	669.	.636	.598	.574	.559	.548	.539
	OCCABION-TO-	.418417	.425417	.439418	.46419	.48942	.526421	.573424	.629427	.696432	.77344

7.62180 BALL 1080 - SYSTEM 1

	200 E <	> > = = = = = = = = = = = = = = = = = =	009 R	900 PE	1000 M	1200 H V	1400 H V	1600 H	1800 V	2000 H C
RANGE	0412	160.1-0	0-2.25	0-4.421	0-7.5	0-11.455	0-16.333	0-22.4	0-29.077	0-38.182
CLUT	. 142-0	.329-0	.587-0	0-96-	1.493-0	2.213-0	3.093-0	4.16-0	5.413-0	6.871-0
GNIM	.408002	.914006	1.563021	2.412061	3.337148	4.1829	4.969493	5.73769	6.483-1.136 7.243-1.614	7.243-1.614
VELOCITY	0041	0097	0182	0317	0492	067	0851	0-1.043	0-1.25	0-1.48
TEMPERATURE	0003	0018	0055	0134	0183	0143	0024	0167	0428	0759
DENSITY	001	900	0192	05	0949	0-1.479	0-2.12	0-2.914	0-3.909	0-5.173
EARTH RATE	.005	.012	.02	.033	.048	.065	.084	104	.127	. 152
SITE ANGLE	0001	0003	0004	0007	001	0015	0021	0029	0037	0047
REFICIA	0	0	0	0	0	0	0	0	0	0
BORESIGHT	•		-	1.	.1	.1	.1	.1.	.1	.1
NOILITION 4	•	-	.1	•	.1	. 1	• 1	.1	.1	1.
S JUMP DISPERSION	.25	.25	.25	.25	.25	.25	.25	.25	.25	.25
ERROING		.3	.3	E.	.3	.3	.3	.3	.3	.3
AIMING	.424849	.212424	.141283	. 106212	.08517	.071141	.061121	.053106	.047094	.042085
RESOLUTION	90.	90.	90.	90.	90.	90.	90.	90.	90.	90.
· APHUNITION DISPERION	.6773	6773.	.6773	.6773	.6773	.6773	.6773	.6773	.6773	£773.
BYSTEM	11.236	11.236 1.274-1.421 1.855-2.419	1.855-2.419	2.718-4.539	3.743-7.623	2.718-4.539 3.743-7.623 4.797-11.60	5.908-16.52	7.126-22.64	5.908-16.52 7.126-22.64 8.484-29.40	10.02-38.61
ROUND-TO-ROUND	.801-1.088	.712801	.694736	.688712	.686701	.683694	.683691	.682688	.682686	.681685
OCCABION-TO- OCCABION	.599587	.599587 1.056-1.173		1.72-2.304 2.629-4.482	3.68-7.591	4.748-11.58	5.868-16.51	7.094-22.63	3.68-7.591 4.748-11.58 5.868-16.51 7.094-22.63 8.457-29.39 9.993-38.60	9.993-38.60

7.6200 BALL MBO - SYSTEM 2

		200 H V	A00	P 600	900 H	1000 H	1200 H V	1400 H V	1600 H V	1800 H	2000 H V
PANGE		0294	0779	0-1.607	0-3.158	0-5.357	0-8.182	0-11.667	0-16.	0-20.769	0-27.273
CLUT		.142-0	.329-0	.587-0	0-96-	1.493-0	2.213-0	3.093-0	4.16-0	5.413-0	6.871-0
WIND		.408002	.914006	1.563021	2.412061	3.337148	4.1829	4.969493	5.73769	6.483-1.136	7.243-1.614
VELOCITY		0041	0097	0182	0317	0492	067	0851	0-1.043	0-1.25	0-1.48
TEMPERATURE		0003	0018	0055	0134	0183	0143	0024	0167	0428	0759
DENSITY		0~.01	900	0192	05	0949	0-1.479	0-2.12	0-2.914	0-3.909	0-5.173
EARTH RATE		.005	.012	.02	.033	.048	.065	180.	. 104	. 127	. 152
BITE ANGLE		0001	0003	900-0	0007	100	0015	0021	0029	0037	0047
RETICLE		0196	026	0357	0526	0714	0909	0-1.111	0-1.333	0-1.538	0-1.818
BORESIGHT		.1						-	.1.		-
NOIT/1708		.1	.1	•1	• 1	.1	.1	• 1	• 1	•	•
NOTERNATION STATES	NOI	.25	.25	.25	.25	.25	. 25	.25	.25	.25	.25
SEROING		.3	6.	.3	€,	€.	.3	€.	€,	€,	.3
AIMING	_ ~	.424849	.212424	.141283	. 106212	71580.	.071141	.061121	.053106	160190	.042085
RESOLUTION		90.	90.	90.	90°	90°	90.	90.	90.	90.	90°
AMMUNITION DISPERION		.6773	6773	.6773	.6773	.6773	.6773	.6773	.6773	.6773	<u>£773.</u>
BYSTEM		11.217	11.217 1.274-1.226	1.855-1.87	2.718 3.362	3.743-5.574	4.797-8.436	4.797-8.436 5.908-11.98 7.126-16.39	7.126-16.39	8.484-21.28	8.484-21.28 10.02-27.93
ROUND-TO-ROUND	!	.801-1.008	.712801	.694736	.688712	.686701	.683694	.683691	.682688	.682686	.681685
OCCABION-TO- OCCABION		599547	.599547 1.056927	1.72-1.719	1.72-1.719 2.629-3.286	3.68-5.529		5.868-11.96	7.094-16.38	4.748-8.408 5.868-11.96 7.094-16.38 8.457-21.27 9.993-77.92	9.993-77.92

7.62180 BALL MSO - SYSTEM 3

	200 H	90 0 N	009 H	900 N	1000 H	1200 H V	1400	1600	1900 N	2000
BLANGE	0098	013	0179	0263	0357	0455	0556	0667	0769	6060
CANT	. 142-0	.329-0	.587-0	0-96-	1.493-0	2.213-0	3.093-0	4.16-0	5.413-0	6.871-0
WIND	.408002	.914006	1.563021	2.412061	3.337148	4.1829	4.969493	5.73769	6.483-1.136 7.243-1.614	7.243-1.614
VELOCITY	0041	0097	0182	0317	0492	067	0851	0-1.043	0-1.25	0-1.48
TEMPERATURE	0003	0018	0055	0134	0183	0143	0024	0167	0428	0759
DENSITY	001	900	0192	05	0949	0-1.479	0-2.12	0-2.914	0-3.909	0-5.173
EARTH RATE	900.	.012	.02	.033	.048	.065	180.	. 104	.127	.152
BITE ANGLE	0001	0003	000	0007	100	0015	0021	0039	0037	0047
RETICLE	0196	026	0357	0526	0714	6060	0-1.111	0-1.333	0-1.538	0-1.018
BORESIGHT	-	1.				-	٠.		-	-
BOLLTION	-	-	-	.1	1.	-	-	+	•	-
AUNP DISPERSION	.25	.25	.25	.25	.25	.25	.25	.25	.25	.25
REPOING	ť.	.3	е.	.3	.3	.3	.3	.3	.3	.3
AIMING	.424849	.212424	.141283	. 106212	.08517	.071141	121190	.053106	.047094	.042085
RESOLUTION	90.	90.	90.	90.	90.	90.	90.	90.	90.	90.
AMMUNITION DISPERION	.6773	.6773	6773	.6773	.6773	.6773	.6773	.6773	.6773	6773
BYSTEM	11.185	11.185 1.274956	1.855974	2.718-1.183	3.743-1.581	4.797-2.105	5.908-2.768	7.126-3.616	5.908-2.768 7.126-3.616 8.484-4.683 10.02-6.077	10.02-6.077
ROUND-TO-ROUND	.801-1.088	.712801	.694736	.688712	.686701	.683694	.683691	.682-,688	.682~.686	.681685
OCCABION-TO- OCCABION	.599471 1.056521	1.056521	1.72637	2.629944	3.68-1.418	3.68-1.418 4.748-1.988 5.868-2.681 7.094-3.55	5.868-2.681	7.094-3.55	8.457-4.633 9.993-6.038	9.993-6.038

7.62191 BALL M80 - SYSTEM 4

		200 H V	¥00	009 H	900 H	1000 M	1200 H V	1400 H V	1600 H V	2 T T T T T T T T T T T T T T T T T T T	2000 R V
~	RANGE	9600	013	0179	0263	0357	0455	0556	0667	0769	6060
9	CANT	.014-0	.033-0	0-650.	0-960-	. 149-0	.221-0	.309-0	.416-0	.541-0	.687-0
-	WIND	.213002	.478006	.617021	1.26061	1.743148	2.18429	2.596493	2.993769	3.387-1.136 3.784-1.614	3.784-1.614
_	VELOCITY	0008	0019	0036	0063	0098	0134	017	0208	025	0296
=*	TEMPERATURE	00005	0004	0011	0027	7600	0029	0005	0034	9800	0152
-	DENBITY	0002	0012	0038	01	019	0296	0424	0583	0782	0-1.035
	EARTH RATE	.005	.012	.02	.033	.048	.065	¥80°	104	121.	. 152
•	SITE ANGLE	0001	0003	000€	0007	001	0015	0021	0029	0037	0047
	RETICLE	•	0	0	0	0	0	0	0	0	0
=4	BORESIGHT	-	-		-	-	٠.	•			•
4!	BOLUTION			1.	٠.	-	1.	•	•	1.	
	JUMP DISPERSION	.25	.25	.25	.25	.25	.25	.25	.25	.25	.25
	ZEROING	E.	.3	.3	.3	.3	.3		.3	e.	е.
~	AIMING	.424849	.212424	.141283	.106212	.08517	.071141	.061121	.053106	.047094	.042085
-	RESOLUTION	90.	90.	90.	90.	90.	90.	90.	90.	90.	90.
- Li	AMENUNITION DISPERION	.6773	6773.	.6773	6773	.6773	6773	.6773	.6773	.6773	.6773
떽	BYSTEM	.927-1.169	.953912	1.151866	1.498876	1.925928	2.337-1.028	2.735-1.191	3.127-1.442	3.524-1.796 3.931-2.298	3.931-2.298
-	ROUND-TO-ROUND	.801-1.088	.712801	.694736	.688712	.686701	.683694	.683691	.682688	.682686	.681685
J	OCCABION-TO-	.467428	.634436	.918456	1.33511	1.799609	2.235758	2.64897	3.052-1.267 3.457-1.659	3.457-1.659	3.871-2.193

XM948 7.62384 ELAP - SYSTEM 1

		200 H V	7 A00	000 H	000 H	1000 M	1200 H V	1400 H V	1600 W W	1800 V	2000 H V	
	RANGE	.019	0494	0-1.008	0-1.931	0-3.684	0-6.632	0-10.5	0-16.	0-22.235	0-30.	
	CLNT	.062-0	. 142-0	.249-0	0-04	.631-0	1.004-0	1.547-0	2.267-0	3.2-0	4.364-0	
	WIND	.251-0	.57001	.979005	1.519015	2.252042	3.162109	4.065228	4.958415	5.866693	6.012-1.099	
	VELOCITY	001	0028	0053	0092	016	0267	0389	0525	0683	087	
	TEMPERATURE	0003	001	0029	007	0158	0272	0334	0343	0304	0221	
	DENSITY	0005	0034	0078	0208	0515	0-1.036	0-1.702	0-2.561	0-3.703	0-5.239	
	BARTH RATE	.003	.007	.013	.021	.032	.048	990.	980.	. 109	.136	
	SITE ANGLE	0-0	0001	0003	0003	0004	0007	0011	0016	0022	003	
	PETICIE	0-0	0-0	0-0	0-0	0-0	0-0	0-0	0-0	0-0	0-0	
	BORESIGHT	•	. 1	•	.1	.1	. 1.		.1.	1.		
	BOLUTION	-	-	-	.1	••	•	.1		.1	.1	
16	JUMP DISPERSION	.25	.25	.25	.25	.25	.25	.25	.25	.25	.25	
	KEROING	.3	.3	.3	.3	.3	.3	.3	.3	.3		
	AIMING	1.94	.97	.647	.485	. 388	.323	772.	.243	.216	. 194	
	RESOLUTION	90.	90.	90.	90.	90.	90.	90.	90.	90.	90.	
•	APPUNITION DISPERION	\$.	5.	ń	ĸ;	19.	v.	ĸ.	ĸ;	ĸ.	'n	
	BYSTEM	2.063-2.056 1.309-1.27	1.309-1.27	1.366-1.368	1.769-2.109	1.366-1.368 1.769-2.109 2.459-3.804 3.397-6.764 4.407-10.68 5.497-16.24 6.718-22.58 8.12-30.495	3.397-6.764	4.407-10.68	5.497-16.24	6.718-22.58	8.12-30.495	
	ROUND-TO-ROUND	2.005	1.093	.83	669.	.636	.598	.575	.559	.548	.54	
	OCCASION-TO- OCCASION	.489457	.72647	1.092-1.095	1.625-1.99	1.092-1,095 1.625-1.99 2.375-3.75 3.344-6.737	3.344-6.737		5.468-16.23	4.37-10.66 5.468-16.23 6.696-22.57 8.102-30.49	8.102-30.49	

XM448 7.6288 81AP - SYSTEN 2

							•				
		200 H C	400	> = 200	900 m	1000 V	1200 H V	1400 H V	1600 V	1800 V	2000 E V
4	FANGE	0136	0353	072	0-1.379	0-2.632	0-4.737	0-7.5	0-11.429	0-15.882	0-21.429
U	CANT	.062-0	. 142-0	.249-0	.40-0	.631-0	1.004-0	1.547-0	2.267-0	3.2-0	4.364-0
#	MIND	.251-0	.57001	.979005	1.519015	2.252042	3.162109	4.065228	4.958415	5.866693	6.812-1.099
>	VELOCITY	100	0028	0053	0092	016	0267	0389	0~.525	0683	087
H	TEMPERATURE	0003	001	0029	007	016	0272	0334	0343	0304	0221
٥	DENSITY	0005	0024	0078	0208	0515	0-1.036	0-1.703	0-2.561	0-3.703	0-5.239
-	EARTH RATE	.003	.007	.013	.021	.032	.048	990.	980.	. 109	. 136
-	SITE ANGLE	0-0	0001	0003	0003	0004	0007	0011	0016	0022	003
-	RETICLE	600	0118	016	023	0351	0526	0714	0952	0-1.176	0-1.429
•	BORESIGHT	-	1.	-	-		1.		.1		-
4	BOLLTION	-	-	-	•	. 1	٠,	. 1	.1	.1	
	JUMP DISPERSION	.25	.25	.25	.25	.25	.25	.25	.25	.25	.25
64	ERDING		6.		.3	.3	. 3	.3	.3	.3	.3
~	AIMING	1.94	76.	.647	.485	.388	.323	772.	. 243	.216	194
=	RESOLUTION	90.	90.	90.	90.	90.	90.	90.	90.	90.	90.
	AMMUNITION	s.	s.	s.	s.	s,	s.	\$.	s,	35	νį
40	SYSTEM	2.063-2.054	2.063-2.054 1.309-1.228	1.366-1.183	1.769-1.635	2.459-2.819		3.397-4.948 4.407-7.777		5.497-11.80 6.718-16.40	8.12-22.163
4	ROUND-TO-ROUND	2.005	1.093	.62	669.	.636	.598	.575	.559	.548	.54
0 0	OCCABION-TO- OCCABION	.489447	.72559	1.092853	1.625-1.478	2.375-2.746	1.625-1.478 2.375-2.746 3.344-4.911	4.37-7.756	4.37-7.756 5.468-11.78 6.696-16.39 8.102-22.16	6.696-16.39	8.102-22.16

XM448 7.62mm slab – system 3

		7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	× 400	009 R	900 A	1000 E V	1200 # V	1400 E V	1600 E V	7 × ×	2000 E
	BANGE	.0045	.0059	.00.09	.0115	.0175	.0263	.0357	.0476	.0589	.0714
	CANT	.062-0	. 142-0	.249-0	0-4-	.631-0	1.004-0	1.547-0	2.267-0	3.2-0	4.364-0
	NIND	.2510	.57001	.979~.005	1.519015	2.252042	3.162109	4.065228	4.958415	5.866693	6.812-1.099
	VELOCITY	001	0028	0053	0092	016	0267	0389	0525	0683	087
	TEMPERATURE	0003	001	0~.039	007	0158	027 2	0334	0343	0304	0221
	DENSITY	9005	0024	0078	0208	0515	0-1.036	6-1.702	0-2.561	0-3.703	0-5.239
	EARTH RATE	.003	.007	.013	.021	.032	.048	990.	980.	. 109	. 136
	SITE ANGLE	0-0	0001	0003	0003	000€	0007	0011	0016	0022	003
	PETICIE	600	0118	016	023	0-,351	0526	0714	0952	0-1.176	0-1.429
	BORESIGHT		•1	•1	•	.1	.1	.1	.1	.1	1.
48	ROILION		• 1		.1	1.	.1	1.	1.	1.	1.
3	JUMP DISPERSION	.25	.25	.25	.25	,25	.25	.25	.25	.25	.25
	SEROING	e.	.3	.3	6.	.3	.3	.3	.3	£°	.3
	AINING	1.94	.97	.647	.485	.388	.323	772.	.243	.216	161.
	RESOLUTION	90.	90.	90.	90.	90.	90.	.06	.06	90.	90.
	AMUNITION	ŵ	S :	\$.	ĸ.	.5	8.	\$.	. 8.	S.	ŝ.
	BYSTEM	2.063-2.05 1.309-1.177	1.309-1.177	1.366942	1.769886	2.459-1.024	2.459-1.024 3.397-1.452	4.407-2.087	5.497-2.958 6.718-4.119	6.718-4.119	8.12-5.701
	ROUND-TO-ROUND	2.005	1.093	.82	669.	.636	. 598	.575	. 559	. 548	.54
	OCCABION-TO-	.489428	.72437	1.092464	1.625544	2.375603	3.344-1.323	4.37-2.006	4.37-2.006 5.468-2.905 6.696-4.082 8.102-5.675	6.696-4.082	8,102-5,675

XM948 7.62nh blad — bybten 4

	200 H V	400 H	600 H V	900 H	1000 H V	1200 H V	1400 H V	1600 H	1800 V M	2000 ER V
RANGE	0045	0059	008	0115	0175	0263	0357	0476	0588	0714
CANT	.006-0	.014-0	.025-0	.04-0	.063-0	. 1-0	.155-0	.227-0	.32-0	.436-0
GNIN	. 131-0	.298001	.511005	.794015	1.177042	1.652109	2.124228	2.59415	3.065693	3.558-1.099
VELOCITY	0003	9000	0011	0018	0032	0053	0078	0105	0137	0174
TEMPERATURE	0001	0003	9000	0014	0032	0054	0067	0069	0061	0044
DENBITY	0001	0005	0016	0042	0103	0207	034	0512	0741	0-1.048
EARTH RATE	.003	.007	.013	.021	.032	.048	990.	. 086	. 109	. 136
SITE ANGLE	0-0	1000	0003	0003	9000	0007	0011	0016	0022	003
RETICLE	0	0	0	0	0	0	0	0	0	0
BORESIGHT	1.	1.	1.	١.	1.	1.	1.	1.	1.	1.
BOLUTION	-	1.	••	-	1.	1.	4.	1.	1.	1.
JUMP DIBPERSION	.25	.25	.25	.25	. 25	.25	.25	.25	.25	. 25
ZEROING	.3	6.	ε.	.3	€*	€*	6.	ۥ	6.	.3
AIMING	1.94	76.	.647	.485	.388	.323	772.	. 243	.216	194
RESOLUTION	90.	90.	90*	.06	90*	90.	90.	90.	90*	90.
AMUNITION DISPERSION	s.	s.	s.	3.	3.	\$.	3.	5.	\$'	\$.
BYSTEM	2.052-2.048 1.207-1.17	1.207-1.171	11.052922	1.138823	1.402789	_	2.245901	2.693-1.081	2.693-1.081 3.159-1.372 3.651-1.825	3.651-1.825
ROUND-TO-ROUND	2.005	1.093	.820	669.	.636	.598	.575	655'	.548	.54
OCCABION-TO- OCCABION	.436418	.51242	.659423	.897435	1.25468	1.707551	2.171694 2.634926 3.111-1.258 3.611-1.743	2.634926	3.111-1.258	3.611-1.743

7.6258 BALL MITO (MATCH) - SYSTEM 1

		200 H <	7 7 N	009 m	> 000 E	1000 E V	1200 H V	1400	1600	1800	2000 H V
	RANGE	0442	0-1.12	0-2.136	0-3.818	0-6.364	0-9.333	0-13.364	0-17.684	0-22.235	0-28.
	CANT	. 16-0	.356-0	.613-0	.951-0	1.404-0	20	2.729-0	3.582-0	4.56-0	S.689-0
	MIND	:377002	.814007	1.332021	1.965051	2.713113	3.414214	4.053357	4.659545	5.252787	5.843-1.095
	VELOCITY	0046	0102	0182	0293	0448	6090	0768	0931	0-1.102	0-1.286
	TEMPRATURE	0003	0008	0024	900	0106	6079	0019	0175	0384	0644
	DENBITY	001	0052	0153	0362	0716	0-1.12	0 -1.583	0-2.136	0-2.81	0-3.642
	ENETH PATE	500.	.012	.02	160.	.044	650.	900.	.093	.112	.133
	BITE ANGLE	1000	0003	0004	0007	001	0014	0019	0025	0031	0039
	REFICIE	0-0	0-0	0-0	0-0	0-0	0-0	0-0	0-0	0-0	0-0
	BOREJIGHT	1.	1.		.1	.1	1.	.1	.1	.1	
Ę	BOLUTION	.1	1.		.1	.1	1.	i.	.1	.1	
50	JUMP DISPERSION	.25	52.	.25	.25	.25	.25	.25	.25	.25	.25
	SEROING	.3	6.	€,	.3	.3	.3	.3	6.	.3	e.
	AIMING	. 424849	.212424	.141283	.106212	.08517	.071141	.061121	.053106	.047094	.042085
	RESOLUTION	90.	90.	90.	90.	90.	90.	90.	90.	90.	90.
	AMMUNITION DISPERION	. 282	.282	.282	.282	.282	.282	.282	.282	.282	.282
	BYSTEM	.777-1.084	1.044-1.30	5 1.557-2.226 2.244-3.887 3.098-6.444 3.991-9.437	2.244-3.887	3.098-6.444	3.991-9.437	4.913-13.50	4.913-13.50 5.899-17.85 6.975-22.46 8.172-28.30	6.975-22.46	8.172-28.30
	ROUND-TO-ROUND	.512897	.357512	.321404	.307358	.301334	.297321	.295313	.293307	.292303	.291301
	C ABION-TO- OCCABION	.584609	.981-1.2	1.524-2.189 2.223-3.87	2.223-3.87	3.083-6.435		4.904-13.49	3.98-9.432 4.904-13.49 5.892-17.85 6.969-22.46 8.167-28.30	6.969-22.46	8.167-28.30

7.62km qlaf hall miss (match) - system 2

	200 H	7 A 400	600 E	900 H	1000 H V	1200 H V	1400 H V	1600 H V	1800 V	2000 H V
RANGE	0316	00	0-1.525	127.2-0	0-4.545	0-6.667	0-9.545	0-12.632	0-15.882	0-20.
CANT	. 16-0	.356-0	.613-0	.951-0	1.404-0	20	2.729-0	3.582-0	4.56-0	5.689-0
MIND	:377002	.814007	1.332021	1.965051	2.713113	3.414214	4.053357	4.659545	5.252787	5.843-1.095
VELOCITY	0046	0102	0182	0293	0448	6090	0768	0931	0-1.102	0-1.286
TEMPERATURE	0003	0008	0024	900	0106	0079	0019	0175	0384	0644
DENSITY	0010	0052	0153	0362	0716	0-1.12	0-1.583	0-2.136	0-2.81	0-3.642
EARTH RATE	.005	.012	.02	.031	.044	.059	900.	.093	.112	.133
SITE ANGLE	0001	0003	000€	0007	010	0014	0019	0025	0031	0039
RETICLE	0211	0267	0339	0455	9090	0741	0909	0-1.053	0-1.176	0-1.333
BORESIGHT		•		•	.1	.1	.1	• 1	.1	٠.
NOILITION 5	1.		.1	.1	• 1	• 1	.1	•	.1	.1
JUMP DISPERSION	.25	.25	.25	.25	.25	.25	.25	.25	.25	.25
EFROING	.3	.3	.3	.3	.3	.3	.3	.3	.3	.3
AIMING	.424849	.212424	.141283	. 106212	.08517	.071141	.061121	.053106	.047094	.042085
RESOLUTION	90.	90.	90.	90.	90.	90.	90.	90.	90.	90.
APHUNITION DISPERION	.282	. 282	.282	.282	.282	.282	.282	.282	.282	.282
BYSTEM	.777-1.06	1.044-1.077	1.557-1.683	2.244-2.859 3.098-4.696	3.098-4.696	3.99-6.853	4.913-9.769	5.899-12.91 6.975-16.24 8.172-20.46	6.975-16.24	8.172-20.46
ROUND-TO-ROUND	.512897	.357512	.321404	.307358	.301334	.297321	.295313	.293307	.292303	.291301
OCCABION-TO- OCCABION	.584565	.981947	1.524-1.634 2.223-2.836 3.083-4.684 3.979-6.845	2.223-2.836	3.083-4.684	3.979-6.845	4.904-9.764	4.904-9.764 5.892-12.91 6.969-16.24 8.167-20.46	6.969-16.24	B. 167-20.46

7.6250 BALL MIIS (MATCH) - SYSTEM 3

		7 7 7	0 2	009 F	009 R	1000 V	1200 H V	1400 E	1600 N	1800 V	2000
•		1 2 2	1	169	0- 227	9- 303		1 20	0- 526	885	
	2.5	16-0	.356-0	.613-0	.951-0	1.404-0	20	2.729-0	3.582-0	4.56-0	5.689-0
3	MIND	.377002	.014007	120	1.965051	2.713113	3.414214	4.053357	4.659545	5.252707	5.843-1.095
5	VELOCITY	0046	0102	0182	0293	0448	6090	0768	0931	0-1.102	0-1.286
*	TEMPERATURE	0003	0008	0024	0060	0106	6079	0019	0175	0384	0644
9	DENSITY	0010	0052	0153	0362	0716	0-1.120	0-1.583	0-2,136	0-2.81	0-3.642
1	EARTH RATE	.005	.012	.02	.031	.044	650.	970.	.093	.112	. 133
18	SITE ANGLE	0001	0003	0004	0007	0010	0014	6100	0025	0031	0039
ä	PETICIE	0211	0267	0339	0455	909.~0	0741	6060	0-1.053	0-1.176	0-1.333
Q	BORESIGNT	•	.1	.1	1.	1.	.1	1.	.,	.1	-
	SOLUTION		1.		.1	1.	1.	1.	••		-
克	JUMP DISPERSION	.25	.25	. 25	.25	.25	.25	.25	.25	.25	.25
H	REBOING	.3	.3	.3	€.	€.	.3	€.	.3	.3	.3
¥	AIMING	.424849	.212424	.141283	.106212	.08517	.071141	.061121	.053106	.047094	.042085
Ž	RESOLUTION	90.	.06	.06	90.	90.	90.	90*	90.	90.	90.
3 6	AMMUNITION	.282	.282	.282	.282	.282	.282	.282	.282	.282	.282
84.	SYSTEM	110.1-777.	.777-1.017 1.044733	1.557733	2.244886	3.098-1.217	3.098-1.217 3.991-1.625		5.899-2.723	5.899-2.723 6.975-3.447 8.172-4.363	8.172-4.363
2	ROUND-TO-ROUND	.512897	.357512	.321404	.307358	.301334	.297321	.295313	.293307	. 292 303	.291301
88	OCCASION-TO- OCCASION	.58448	.981524	1.524612 2.22381	2.22381	3.083-1.17	3.98-1.593	3.98-1.593 4.904-2.106 5.892-2.706 6.969-3.434 8.167-4.353	5.892-2.706	6.969-3.434	8.167-4.353

7.6256 BALL MIIS (MATCH) - SYSTEM 4

		200	> =	009	900 H	1000 V	1200 H V	1400	1600 H V	1900 M	7 000 E 7000
PANGE		0105	0133	0169	0227	0303	0370	0455	0526	0588	0667
CANT		.016-0	.036-0	.061-0	0-560.	. 14-0	.2-0	.273-0	.358-0	.456-0	0-695.
QNI M		. 197002	.425007	.696021	1.027051	1.417113	1.783214	2.117357	2.434545	2.743787	3.052-1.095
VELOCITY		0009	.03	0036	0059	00	0122	0154	0186	022	0257
TEMPERATURE	282	0001	0003	0005	0012	0021	0016	0004	0035	0077	0129
DENBITY		0003	001	0031	0072	0143	0224	0317	0427	0562	0728
EARTH RATE	Ę	.005	.012	.02	.031	.044	.059	.076	.093	. 112	. 133
SITE ANGLE	1	0001	0003	0004	0007	001	0014	0019	0025	0031	0039
NETICLE		•	0	9	0	0	0	0	0	•	0
TES I STROE	t	1.	1.	•	•		•	٠.	+		-
ROILLION 5	_	•		•			•			•	-
CONTRACTOR OF THE STORM	PERSION	.25	.25	.25	.25	.25	.25	.25	.25	.25	.25
SEROING		E.	.3	.3	.3	.3	.3	.3	.3		.3
AIMING		.424849	.212424	.141283	.106212	.08517	.071141	.061121	.053106	.047094	.042085
RESOLUTION	5	90.	90.	90.	90.	90.	90.	90.	90.	90.	90.
AMMUNITION DISPERSON	75 74	. 282	.282	.282	.282	.282	.282	.282	.282	.282	. 282
BYSTEM		.688994	.695674	.874606	1.155604	1.514648	1.866726	2.196855	2.514-1.034	2.514-1.034 2.829-1.271 3.148-1.594	3.148-1.594
ROUND-TO-ROUND	- ROUND	.512897	.357512	.321404	.307358	.301334	.297321	.295313	.293307	.292303	.291301
OCCABION-TO- OCCABION	-04-1	.46429	.596438	.813452	1.113486	1.484555	1.843651	2.176796	2.497987	2.814-1.234	2.814-1.234 3.135-1.565

APPENDIX C BALLISTIC DATA FROM BRL

The following ballistic data was calculated at the Ballistics Research Laboratory in Aberdeen, MD.

.50 CALIBER M20 APIT

.50 CALIBER M8 API

Range	Super Elev	dR/dTh	نه	dH Vel	dH Temp	dH Density	dH Range Wind	dD Cross Wind	Vert Disp	Hor Disp
(m)	(mil)	(m/m11) (sec)	(sec)	(m)	(m)	(m)	(m)	(m)	(mils)	(mils)
200.0 400.0 600.0 800.0 1000.0 1400.0 1600.0 2000.0	1.3 2.9 4.7 6.9 9.5 12.6 16.4 21.1	132.0 113.0 96.0 81.0 68.0 56.0 46.0 32.0 28.0	0.0 0.0 0.5 1.1 1.5 4.3 3.0 5.0 5.0	0.0006 0.0025 0.0063 0.0124 0.0217 0.0353 0.0548 0.0822 0.1157	0.0000 0.0002 0.0009 0.0026 0.0129 0.0249 0.0446	0.0002 0.0019 0.0075 0.0209 0.0483 0.0998 0.1919 0.3373	0.0000 0.0003 0.0014 0.0039 0.0196 0.0390 0.0737 0.1289	0.0131 0.0548 0.1302 0.2446 0.4052 0.6203 0.9011 1.2564 1.6615	1.0000000000000000000000000000000000000	1.50 1.50 1.50 0.50 1.50 1.50

.50 CALIBER M33 BALL

Range	Super	dR/dTh	L.	dH Ve1	dH	dH Density	dH Range	dD	Vert Disp	Hor
					•		Wind	Wind	•	•
(m)	(m11)	(m/mil)	(sec)	(m)	(m)	(m)	(m)	(m)	(mils)	(mils)
200.0	1.3	133.0	0.2	9000.0	0.0000	0.0002	0.0000	0.0127	1.00	1.50
400.0	2.9	114.0	0.5	0.0025	0.0003	0.0019	0.0003	0.0535	1.00	1.50
0.009	4.7	97.0	8.0	0.0063	0.0011	0.0073	0.0013	0.1270	1.00	1.50
800.0	8.9	82.0	1.1	0.0124	0.0031	0.0203	0.0036	0.2389	1.00	1.50
1000.0	9.6	0.69	1.5	0.0218	0.0072	0.0471	0.0086	0.3963	1.00	1.50
1200.0	12.5	57.0	1.9	0.0355	0.0149	0.9076	0.0185	0.6078	1.00	1.50
1400.0	16.2	47.0	2.4	0.0552	0.0284	0.1876	0.0370	0.8842	1.00	1.50
1600.0	20.8	38.0	3.0	0.0826	0.0475	0.3321	0.0701	1.2340	1.00	1.50
1800.0	26.5	32.0	3.6	0.1173	0.0579	0.5219	0.1239	1.6411	1.00	1.50
2000.0	33.0	28.0	4.3	0.1572	0.0475	0.7750	0.2022	2.0857	1.00	1.50

.50 CALIBER SLAP XM903

Range	Super	dR/dTh		ЧН	HP	ЧН	HP	QΡ	Vert	Hor
	Elev			Vel	Temp	Density	Range	Cross	Disp	Disp
		•					n i i	DIITM		
(B)	(mil)	(m/mil)	(sec)	(B)	(B)	(m)	(B)	(m)	(mils)	(mils)
200.0	0.7	255.0	0.2	0.0002	0000.0	0.0001	0.000	0.0049	0.50	0.50
400.0	1.5	236.0	7.0	0.0010	0.0002	0.0005	0.0000	0.0203	0.50	0.50
0.009	2.3	217.0	0.5	0.0024	0.0007	0.0018	0.0001	0.0474	0.50	0.50
800.0	3.3	198.0	8.0	0.0045	0.0019	0.0047	0.0004	0.0877	0.50	0.50
1000.0	4.3	181.0	0.1	920010	0.0040	0.0103	0.0009	0.1428	0.50	0.50
1200.0	5.4	164.0	1.2	0.0	0.0075	0.0198	0.0018	0.2147	0.50	0.50
1400.0	9.9	148.0	1.5	0.0171	0.0132	0.0353	0.0032	0.3056	0.50	0.50
1600.0	8.0	133.0	1.7	0.0242	0.0217	0.0594	0.0057	0.4148	0.50	0.50
1800.0	9.5	119.0	2.1	0.0334	0.0344	0.0959	0.0095	0.5552	0.50	0.50
2000.0	11.2	105.0	2.4	0.0450	0.0526	0.1503	0.0155	0.7208	0.50	0.50

y grange	Super	ak/ain	u	dH Vel	dH Temp	dH Density	dH Range	dD Cross	Vert Disp	Hor Disp
							Wind	Wind	•	•
(B)	(m11)	(m/m11)	(sec)	(m)	(m)	(m)	(m)	(m)	(mils)	(m11s)
200.0	1.6	102.0	0.3	0.0008	0.0001	0.0004	0.0001	0.0239		0.68
400.0	3.7	77.0	9.0	0.0038	0.0014	0.0047	0.0007	0.1072		0.68
0.009	9.9	26.0	1.0	0.0107	0.0065	0.0226	0.0037	0.2749		0.68
800.0	10.8	38.0	1.5	0.0249	0.0211	0.0786	0.0142	0.5654	_	0.68
1000.0	16.8	28.0	2.2	0.0483	0.0359	0.1863	0.0433	0.9779	_	0.68
1200.0	24.9	22.0	2.9	0.0789	0.0337	0.3484	0.1019	1.4700	Ī	0.68
1400.0	34.8	18.0	3.7	0.1169	0.0066	0.5829	0.2023	2.0387	_	0.68
1600.0	8.94	15.0	4.6	0.1638	0.0526	0.9156	0.3608	2.6868	_	0.68
1800.0	6.09	13.0	5.6	0.2209	0.1513	1.3817	0.5991	3,4198	_	0.68
2000.0	77.3	11.0	9.9	0.2905	0.2979	2.0314	0.9461	4.2454	0.68	0.68

7.62mm SLAP XM948

Range	Super	dR/dTh	T L	dH Vel	dH Temp	dH Density	dH Range	dD Cross	Vert Disp	Hor Disp
(B)	(mil)	(m/mil) (sec)	(sec)	(m)	(m)	(n)	(E)	(E)	(m11s)	(mils)
200.0	0.7	221.0	0.5	0.0002	0.000	0.0002	0000.0	0.0147	0.50	0.50
0.004	1.6	170.0	7.0	0.0011	0.0008	0.0019	0.0001	0.0668	0.50	0.50
0.009	2.8	125.0	9.0	0.0031	0.0034	0.0092	0.0008	0.1721	0.50	0.50
800.0	4.5	87.0	1.0	0.0072	0.0110	0.0327	0.0034	0.3562	0.50	0.50
1000.0	7.1	57.0	1.4	0.0157	0.0310	0.1011	0.0122	0.6601	0.50	0.50
1200.0	11.3	38.0	2.0	0.0314	0.0641	0.2442	0.0382	1.1121	0.50	0.50
1400.0	17.4	28.0	2.8	0.0534	0.0919	0.4678	0.0936	1.6678	0.50	0.50
1600.0	25.5	21.0	3.6	0.0825	0.1079	0.8047	0.1946	2.3248	0.50	0.50
1800.0	36.0	17.0	4.5	0.1207	0.1076	1.3088	0.3658	3.0946	0.50	0.50
2000.0	49.1	14.0	5.6	0.1708	0.0866	2.0574	0.6443	3.9926	0.50	0.50
62										

7.62mm BALL M118 NATIONAL MATCH

Range	Super	dR/dTh	4	dh Ve1	dH Temp	dH Density	dH Range Wind	dD Cross Wind	Vert Disp	Hor Disp
(m)	(mil)	(m/m11)	(sec)	(m)	(m)	(m)	(m)	(m)	(mils)	(mils)
0 000	8	95.0	0.3	0.0009	0.0001	0.0004	0.0001	0.0221	0.282	0.282
0.004	0.4	75.0	9.0	0.0040	900000	0.0041	0.0008	0.0954	0.282	0.282
0.004	9	59.0	1.0	0.0107	0.0028	0.0180	0.0037	0.2343	0.282	0.282
800.0	10.7	0.44	1.5	0.0230	0.0095	0.0569	0.0120	0.4608	0.282	0.282
1000	15.8	33.0	2.1	0.0440	0.0208	0.1406	0.0331	0.7951	0.282	0.282
1200	22.5	27.0	2.7	0.0718	0.0186	0.2640	0.0754	1,2006	0.282	0.282
1400.0	30.7	22.0	3.4	0,1056	0.0052	0.4352	0.1463	1,6630	0.282	0.282
1600.0	40.3	19.0	4.2	0.1462	0.0551	0.6710	0.2554	2.1848	0.282	0.282
1800.0	51.3	17.0	5.0	0.1948	0.1358	0.9930	0.4152	2.7702	0.282	0.282
2000.0	64.0	15.0	0.9	0.2525	0.2528	1.4303	0.6418	3,4244	0.282	0.282
ŧ										

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